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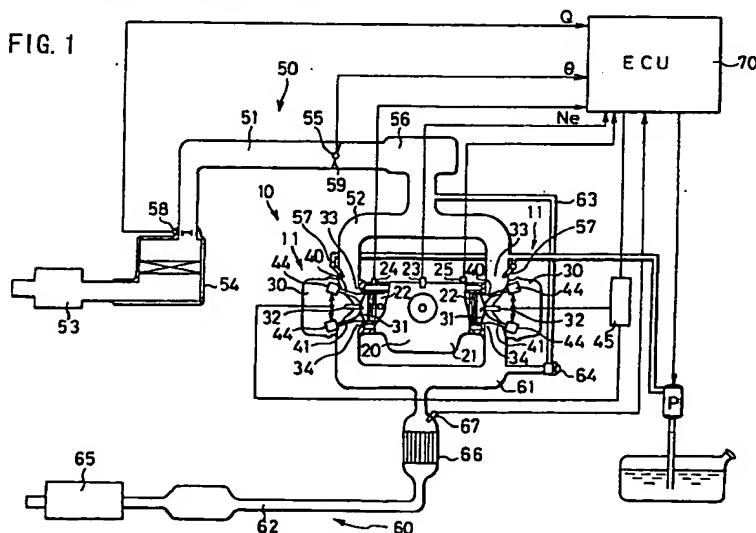
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(54) Electromagnetically operated valve control system and the method thereof

(57) The system and method for controlling an electromagnetically operated valve driving mechanism comprises an actuator (44), an actuator drive circuit (45), a lift sensor (170), an actuator control apparatus (210), and a micro-computer (71). The actuator (44) includes a valve opening solenoid (132) and a valve closing solenoid (131). The actuator control apparatus (210) generates signals for energizing and deenergizing the valve opening solenoid (132) and the valve closing solenoid

(131) based on control data supplied from the lift sensor (170) and the micro-computer (71). The system is able to control the electromagnetically operated valve driving mechanism only by the actuator control apparatus (210) without using the micro-computer (71) in a precise and sophisticated manner, so that the burden on the micro-computer (71) can be relieved.

FIG. 1



Description

BACKGROUND OF THE INVENTION

1. Field of the invention

The present invention relates to a system and method for controlling electromagnetically operated intake and exhaust valves of an internal combustion engine.

2. Prior Art

An electromagnetically operated valve mechanism is of a valve driving technique in which a valve body is operated by generating magnetic force in an actuator by supplying current thereto and there are numerous proposed techniques relating to that mechanism. The electromagnetically operated valve mechanism is characterized in that the construction of the valve driving mechanism can be simplified because of the absence of a cam mechanism and further the valve opening and closure timing of the intake and exhaust valves can be selectively established according to engine operating conditions, this enabling a wide range of selection of engine output characteristics and further leading to an improvement of fuel economy.

Fig. 14 is a schematic cross sectional view showing an example of an electromagnetically operated valve mechanism according to the prior art. The shown electromagnetically operated valve mechanism is an example employed on the exhaust valve side. With respect to the intake valve side, its detailed description will be omitted because of a similar construction.

As shown, generally, the electromagnetically operated valve mechanism 110 comprises a valve body 120, an electromagnetic force generating section 130, a biasing section 140 and an armature 150. Also the valve body 120 comprises a valve 121 and a valve stem 122 and it is reciprocatably supported by a stem guide 161 provided in a cylinder head 160.

The valve 121 is formed so as to have a close contact with a valve seat 164 provided around an exhaust port end 163. Further, the valve stem 122 is connected at the top end thereof with the armature 150 fabricated of magnetic material.

The electromagnetic force generating section 130 is constituted by an electromagnetic solenoid 131 for closing a valve (hereinafter, referred to as valve closing solenoid, an electromagnetic solenoid 132 for opening a valve (hereinafter, referred to as valve opening solenoid), a first core 133 for the valve closing solenoid 131 and a second core 134 for the valve opening solenoid 132. The armature 150 is inserted between the first and second cores 133, 134 so as to move vertically therebetween.

The biasing section 140 comprises a spring 141 for opening a valve (hereinafter, referred to as valve open-

ing spring) and a spring 142 for closing a valve (hereinafter, referred to as valve closing spring). The valve opening spring 141 is provided between the first core 133 and the valve stem 122 so as to bias the valve body 120 in the opening direction (downward direction in this drawing) with a specified biasing force. Further, the valve closing spring 142 is provided between the second core 134 and the armature 150 so as to bias the valve body 120 in the closing direction (upward direction in this drawing) with a specified biasing force.

When the valve closing solenoid 131 and the valve opening solenoid 132 are both deenergized, the valve opening spring 141 and the valve closing spring 142 have such a biasing force respectively that the armature 150 is sustained at about the mid-point between the first and second cores 133, 134. Therefore, when either of these solenoids 131, 132 is energized, the armature 150 can be attracted with less attraction force.

Describing an operation of this valve mechanism briefly, first, when the valve closing solenoid 131 is energized, an electromagnetic force is generated in the valve closing solenoid 131 to attract the armature 150 in the direction of the valve closing solenoid 131 against the biasing force of the valve opening spring 141 and as a result the valve body 120 travels in the closing direction (upward direction in this drawing) until the valve 121 comes into close contact with the valve seat 164. Thus, the combustion chamber 165 is sealed up against the exhaust port 162.

When the valve opening solenoid 132 is energized, the armature 150 is attracted toward the valve opening solenoid 132 to move the valve body 120 in the opening direction (downward direction) until the valve 121 is fully open.

Fig. 14 shows a state in which the electromagnetic force generating section 130 is deenergized and the armature 150 is positioned at the mid-point of the first core 133 and the second core 134.

JP-A-61-76713 discloses an electromagnetically operated valve control system in which the valve speed immediately before seating on the valve seat is reduced to alleviate an impact when seated. Further, JP-A-7-224624 discloses an electromagnetically operated valve train apparatus wherein the lift amount is detected by a lift sensor.

In applying the foregoing electromagnetically operated valve train system to a multi-cylinders engine, the current control must be performed per respective electromagnetic solenoids provided on each cylinder. In case of an electromagnetically operated valve train system as shown in Fig. 14, two electromagnetic solenoids, one for opening the valve and the other for closing the valve, are employed. Therefore, for example, in case of a four cylinders-four valves engine, thirty-two (32) electromagnetic solenoids must be controlled independently.

In order to generate signals for driving these numerous electromagnetic solenoids in the micro-com-

puter in a timely manner, it is necessary to increase the number of channels and to enlarge the computing capacity of the micro-computer. Further, when performing such a fine valve opening and closing control as proposed in JP-A-61-76713 or JP-A-7-224624, still greater burden is charged on the micro-computer.

Therefore, in order to perform the above-mentioned valve opening and closing control, a high performance computer must be used, this resulting in a cost increase of the system.

SUMMARY OF THE INVENTION

With the above described problem in mind, it is an object of the present invention to provide an electromagnetically operated valve control system capable of performing a more precise and more sophisticated valve driving control with less burden on the micro-computer.

In order to achieve the above mentioned object, the electromagnetically operated valve control system comprises: control data generating means for generating a control data based on operating conditions of the engine, valve position detecting means for detecting reference positions of the valve body, valve closing acceleration means for energizing a valve closing solenoid when the valve body passes a first reference position apart from the fully open position and for deenergizing a valve closing solenoid when the valve body passes a second reference position closer to the fully closed position than the first reference position, valve seating velocity adjusting means for energizing the valve closing solenoid when the valve body passes a third reference position closer to the fully closed position than the second reference position and for deenergizing the valve closing solenoid when the valve body passes a fourth reference position closer to the fully closed position than the third reference position so as to adjust a seating velocity of the valve body, valve closing hold means for repeatedly energizing and deenergizing the valve closing solenoid when the valve body passes the fourth reference position and for deenergizing the valve closing solenoid when a first specified period has elapsed since the valve body passes the fourth reference position, valve opening acceleration means for energizing the valve opening solenoid when the valve body passes a fifth reference position apart from the fully closed position and for deenergizing the valve opening solenoid when the valve body passes a sixth reference position closer to the fully open position than the fifth reference position, valve opening velocity adjusting means for energizing the valve opening solenoid when the valve body passes a seventh reference position closer to the fully open position than the sixth reference position and for deenergizing the valve opening solenoid when the valve body passes an eighth reference position closer to the fully open position than the seventh reference position so as to adjust an opening velocity of the valve

body, and valve opening hold means for repeatedly energizing and deenergizing the valve opening solenoid when the valve body passes the eighth reference position and for deenergizing the valve closing solenoid when the second specified period has elapsed since the valve body passes the eighth reference position so as to hold the valve body at the fully open position.

BRIEF DESCRIPTION OF THE DRAWINGS

By way of example only, a specific embodiment of the present invention will now be described, with reference to the accompanying drawings, in which:

Fig. 1 is an overall schematic view showing an electromagnetically operated valve control system according to the present invention;

Fig. 2 is a schematic view showing a construction of an electronic control unit (ECU) shown in Fig. 1;

Fig. 3 is a schematic view showing an exhaust valve and an actuator illustrated in Fig. 1;

Fig. 4 is a basic functional block diagram of an electromagnetically operated valve control system according to the present invention;

Fig. 5 is a block diagram of an electromagnetically operated valve control system according to a first embodiment of the present invention;

Fig. 6 is a timing chart showing an ON-OFF operation of miscellaneous control signals according to a first embodiment;

Fig. 7 is a timing chart showing an closing and opening operation of a valve body in conjunction with the ON-OFF timing of valve closing and opening solenoids according to a first embodiment;

Fig. 8 is a block diagram of an electromagnetically operated valve control system according to a second embodiment of the present invention;

Fig. 9 is a timing chart showing an ON-OFF operation of miscellaneous control signals according to a second embodiment;

Fig. 10 is a block diagram of an electromagnetically operated valve control system according to a third embodiment of the present invention;

Fig. 11 is a timing chart showing an ON-OFF operation of miscellaneous control signals according to a third embodiment;

Fig. 12 is a block diagram of an electromagnetically operated valve control system according to a fourth embodiment of the present invention;

Fig. 13 is a timing chart showing an ON-OFF operation of miscellaneous control signals according to a fourth embodiment; and

Fig. 14 is a schematic view of an electromagnetically operated valve mechanism according to the prior art.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

Referring now to Fig. 1, numeral 10 denotes a horizontally opposed engine, numeral 50 denotes an air intake passageway, and numeral 60 denotes an exhaust passageway. The engine 10 has a plurality of cylinders 11 and it comprises a cylinder block 20 and a cylinder head 30. The cylinder block 20 has an oil pan 21 at the central portion thereof, a plurality of cylinder bores (not shown) on the left and right sides thereof and a plurality of pistons 22 are reciprocatably inserted into the cylinder bores through a crank shaft (not shown) and a connecting rod (not shown).

Further, in the cylinder block 20 there are provided with a crank angle sensor 23 for detecting engine speed N_e and crank angle, a coolant temperature sensor 24 for detecting coolant temperature and a knock sensor 25 for detecting knocking. These sensors act as detecting engine operating conditions to be used for determining the valve opening and closing timing.

The cylinder head 30 has a combustion chamber 31 for each cylinder 11 and a spark plug 32 is projected into the combustion chamber 31. The spark plug 32 serves as igniting mixture gas supplied to the combustion chamber 31 with high voltage applied by an ignitor (not shown) and an ignition coil (not shown) at a specified ignition timing.

Further, the cylinder head 30 has an air intake port 33 communicating with the air intake passageway 50 for feeding mixture gas to the combustion chamber 31 and an exhaust port 34 communicating with the exhaust passageway 60 for discharging exhaust gases.

Further, there are provided with an intake valve 40 for communicating or shutting off the passage between the air intake port 33 and the combustion chamber 31 and an exhaust valve 41 for communicating or shutting off the passage between the exhaust port 34 and the combustion chamber 31. The communication is performed by means of opening the passage between the air intake port 33 or the exhaust port 34 and the combustion chamber 31 by moving the intake valve 40 or the exhaust valve 41 in the direction of the combustion chamber 31 and the shutting-off is performed by means of closing the passage between the air intake port 33 or the exhaust port 34 and the combustion chamber 31 by returning the intake valve 40 or the exhaust valve 41 in the opposite direction.

Further, the cylinder head 30 has an actuator 44 for opening and closing the intake valve 40 and the exhaust valve, respectively. The actuator 44 opens and closes the intake valve 40 and the exhaust valve 41 by passing and shutting off current supplied from an actuator drive circuit 45.

The air intake passageway 50 is constituted by an intake passage 51 and an intake manifold 52. The intake passage 51 has, in the order arranged from upstream to downstream, an intake chamber 53 for

reducing pulsation of intake air, an air cleaner 58 for removing dusts in the air and a throttle valve 55 for controlling the intake air amount Q according to the amount of depression of an accelerator pedal (not shown).

The intake manifold 52 has a surge tank 56 downstream of the throttle valve 55 and branches at the downstream portion of the surge tank 56 into a plurality of manifolds communicating with an intake port 33 for each cylinder 11. Further, a fuel injector 57 is provided at the downstream end of each manifold so as to inject fuel towards the intake port 33.

The exhaust passageway 60 is constituted by an exhaust manifold 61 and an exhaust passage 62. The exhaust manifold 61 has such a configuration as enabling to collect exhaust gas from each cylinder. Further, there is provided with an EGR passage 63 having a smaller passage area than that of the intake manifold 52 or the exhaust manifold 61 so as to communicate between both branch points of the intake manifold 52 and the exhaust manifold 61 and further, on the way of the EGR passage 63 there is provided with an EGR valve 64 driven by a stepping motor, for example.

The exhaust passage 62 is connected upstream thereof with the exhaust manifold 61 and connected downstream thereof with a muffler 65 provided at the rear (not shown) of the vehicle. Further, there is provided with a three-way catalyst 66 at the upstream portion of the muffler 65. Further, there is provided with an oxygen sensor 67 at the immediately upstream portion of the three-catalyst 66 for finding the air-fuel ratio by detecting an oxygen density in exhaust gas.

Further, in order to detect engine operating conditions, there are provided with an air-flow meter 58 for detecting the intake air amount Q and a throttle opening angle sensor 59 for detecting a throttle opening angle θ of the throttle valve 55 in the air intake passageway 50.

Further, the control system has an electronic control unit (hereinafter referred to as ECU) 70 to which signals from the above described sensors are input and from which control signals are output to miscellaneous control means.

Fig. 2 is a schematic view showing an internal construction of the ECU 70. The ECU 70 is mainly composed of a micro-computer 71 which is a central processing and calculating means and a constant voltage circuit 72 for supplying a stable electric power to miscellaneous components, a drive circuit 73 and an A/D converter 74 are incorporated therein.

The micro-computer 71 comprises an input/output interface 71a for inputting detected signals from miscellaneous sensors of the engine 10 and for outputting control signals to miscellaneous control means, a CPU 71c as a major computing apparatus, a ROM 71d in which the control program or fixed data are memorized, a RAM 71e in which processed data of signals from miscellaneous sensors and data processed in the CPU 71c are stored, a backup RAM 71f for accommodating learned data and the like, a timer 71g and a bus line 71h

for connecting these components with each other.

Fig. 3 is a schematic explanatory diagram of the exhaust valve 41 and the actuator 44 shown in Fig. 1. The construction and components of the valve mechanism shown in Fig. 1 which are almost the same as those shown in Fig. 14 are denoted by identical reference numerals and are not described in detail.

As shown, on the first core 133 there is provided a lift sensor 170 for sensing the open and closed state of the valve body 120, namely, the amount of lift of the valve body 120 and for outputting the amount of lift as an analogue signal "v". The lift sensor 170 is constituted of a main body 171 and a sensor shaft 172. The sensor shaft 172 is connected at the lower end thereof with the top end 123 of the valve body 120 and travels vertically being interlocked with the opening and closing movement of the valve body 120. The main body 171 detects the travelling amount of the sensor shaft 172 as a lift amount of the valve body 120 and outputs the lift amount as an analogue signal "v".

The lift sensor 170 is one kind of displacement meter which detects the position of the valve body 120 by measuring a travelling distance from the reference point. In this embodiment, the lift sensor 170 is a non-contacting type displacement meter using eddy current. Other types of displacement meter such as using laser, ultrasonic, infrared and the like may be employed.

Fig. 4 is a basic functional block diagram for explaining the feature of the present invention. In which, the micro-computer 71 calculates miscellaneous data of the engine and generates control data such as a valve hold period. An actuator control apparatus 210 is for energizing and deenergizing the actuator 44 through the actuator drive circuit 45 based on the control data from the micro-computer 71 and on the analogue signal from the lift sensor 170. Therefore, the electromagnetically operated valve control system according to the present invention is characterized in that the valve drive control is relied only upon the actuator control apparatus 210 which is provided separately from the micro-computer 71.

Next, a first embodiment will be described with reference to Fig. 5, Fig. 6 and Fig. 7.

As shown in Fig. 5, the electromagnetically operated valve control system incorporates the micro-computer 71 and the actuator control apparatus 210. The actuator control apparatus 210 comprises a digital-to-analogue conversion circuit (hereinafter, referred to as DA conversion circuit) 211, a comparison circuit 212, a timer circuit 213 and a valve control signal output section 214.

Further, the actuator drive circuit 45 comprises a valve closing solenoid drive circuit 45a and a valve opening solenoid drive circuit 45b.

The micro-computer 71 outputs a digital data signal and a digital channel signal to the DA conversion circuit 211. Further, the micro-computer 71 outputs a valve hold time data to the timer circuit 213 and a valve hold cur-

rent control signal to the valve control signal output section 214, respectively.

The digital data signal and the digital channel signal are used for outputting specified reference analogue signals v1 to v8 to specified channels. The valve hold time data signal is a signal for indicating a period during which the valve is held at the fully open position or at the fully closed position. The valve hold current control signal is a signal for holding the valve at the fully open or fully closed position.

The DA conversion circuit 211 outputs specified reference analogue signals v1 to v8 to specified channels based on the digital data signal and the digital channel signal input from the micro-computer 71. These analogue signals v1 to v8 are compared to an analogue signal "v" which is output when the valve body 120 is at a specified lift position.

The comparison circuit 212 compares the reference analogue signals v1 to v8 output from the DA conversion circuit 211 with the analogue signal "v" output from the lift sensor 170 to detect the open and closed state of the valve body 120. In the comparison circuit 212, when a "+" input signal is larger than a "-" input signal, a high level signal (hereinafter, referred to as Hi) is output and on the contrary when a "+" input signal is smaller than a "-" input signal, a low level signal (hereinafter, referred to as Lo) is output.

In the first embodiment and embodiments which will be described hereinafter, the reference analogue signals v1 to v8 are generated in the DA conversion circuit 211, however other generating means such as a resistive divider and the like may be introduced.

Accordingly, as a result of the comparison of the analogue signal "v" with the reference analogue signals v1 to v8, the current position of the valve body 120 can be known. Further, it is possible to know the travelling state of the valve body 120 by investigating its positional change. The travelling state of the valve body 120 is output to the timer circuit 213 and the valve control signal output section 214, respectively.

The timer circuit 213 is constituted by a one-shot pulse generating circuit with two channels. When a specified input signal is input from the comparison circuit 212, being triggered by a leading edge of the input signal, a specified signal based on the valve holding time data input from the micro-computer 71 is output to the valve control signal output section 214 for a specified period.

The valve control signal output section 214 is a logical circuit constituted by an AND circuit, an OR circuit, an inverter circuit and a flip-flop circuit and it outputs a valve closing signal s14 and a valve opening signal s26 to the valve closing solenoid drive circuit 45a and the valve opening solenoid drive circuit 45b, respectively according to the position of the valve body 120.

Further, the valve closing solenoid drive circuit 45a and the valve opening solenoid drive circuit 45b supplies current to the valve closing solenoid 131 and the

valve opening solenoid 132 in the actuator 44 based on the valve closing signal s14 and the valve opening signal s26, respectively.

Next, an opening and closing operation of the valve body 120 according to the first embodiment will be described. Fig. 7 is a diagram showing the movement of the valve body 120 and the timing of the valve driving signals. The shown lift sensor signal is a signal "v" which is detected by a lift sensor 170 to be compared with shown specified positions v1, v2, v3, etc. The valve closing solenoid drive signal indicates a signal s14 (shown in Fig. 6) to be output from the valve control signal output section 214 to the valve closing solenoid circuit 45a and the valve opening solenoid drive signal indicates a signal s26 (shown in Fig. 6) to be output from the valve control signal output section 214 to the valve opening solenoid circuit 45b.

First, when the valve opening solenoid drive signal s26 is turned OFF at a time "j" in Fig. 7, the valve opening solenoid 132 is deenergized. Thus, the armature 150 loses attraction force and as a result the valve body 120 starts to move towards the closing side by the spring force of the valve closing spring 142. After that, when the analogue signal "v" of the lift sensor 170 becomes larger than a reference analogue signal v1, the valve closing signal s14 is turned ON at a time "a" in Fig. 7. Therefore, the valve closing solenoid 131 is energized, the armature 150 is attracted by the valve closing coil 131 and the valve body 120 continues to move towards the closing side against the biasing force of the valve opening spring 141.

Then, when the analogue signal "v" of the lift sensor 170 becomes larger than a reference analogue signal v2, the valve closing signal s14 is turned OFF at a time "b" in Fig. 7. Thus, a valve closing acceleration signal "A", namely, a signal for accelerating the armature 150 and seating the valve body 120 at an approximate constant velocity, has been formed.

When the valve closing solenoid drive signal s14 is turned OFF, the valve closing solenoid 131 is deenergized and the armature 150 loses attraction force. As a result, the armature 150 is stopped to be attracted, however, inertia force allows the valve body 120 to continue to move toward the closing side.

Further, when the analogue signal "v" of the lift sensor 170 becomes larger than a reference analogue signal v3, the valve closing solenoid drive signal s14 is turned ON at a time "c" in Fig. 7. Thus, the valve closing solenoid 131 is energized and attraction force is generated in the armature 150 to accelerate again the valve body 120 toward the closing side. Further, when the analogue signal "v" of the lift sensor 170 becomes larger than a reference analogue signal v4, the valve closing solenoid drive signal s14 is turned OFF at a time "d" in Fig. 7. Thus, a valve seating velocity adjusting signal "B", namely, a signal for making a fine adjustment to the valve speed at which the valve body 120 is seated on the valve seat 164, has been formed between the

time "c" and the time "d".

When the valve closing solenoid drive signal s14 is turned OFF at a time "d", being triggered by a trigger signal (channel 1 signal) at a trailing edge of the signal, a valve closing hold signal "C" composed of a PWM signal is output during a specified period t5 between the time "d" and the time "e". This specified time t5 is determined in the microcomputer 71 according to engine operating conditions. As a result, the valve body 120 is kept fully closed until the time "e".

Describing an opening operation of the valve body 120, when the valve closing solenoid drive signal s14 is turned OFF at a time "e" in Fig. 7, the valve closing solenoid 131 is deenergized and the valve body 120 starts to move toward the opening side by the valve opening spring 141.

When the analogue signal "v" of the lift sensor 170 becomes smaller than a reference analogue signal v5 being accompanied by the movement of the valve body 120, the valve opening solenoid drive signal s26 is turned ON at a time "f" shown in Fig. 7. As a result, the valve body 120 continues to move toward the opening side by the attracting force of the valve opening solenoid 132. Then, when the analogue signal "v" becomes smaller than a reference analogue signal v6, the valve opening solenoid drive signal s26 is turned OFF at a time "g" shown in Fig. 7. Thus, a valve opening acceleration signal "D", namely, a signal for accelerating the valve body 120 to an approximate constant speed, has been formed between "f" and "g".

Since the inertia force is applied to the valve body 120 in the opening direction, the valve body 120 continues to move to the opening side. Then, when the analogue signal "v" becomes smaller than a reference analogue signal v7, the valve opening solenoid drive signal s26 is turned ON again at a time "h" shown in Fig. 7.

Then, an attracting force is generated in the valve opening solenoid 132 and the valve body 120 continues to move toward the opening side. When the analogue signal "v" becomes smaller than a reference analogue signal v8, the valve opening solenoid drive signal s26 is turned OFF at a time "i" shown in Fig. 7. Thus, a valve opening velocity adjusting signal "E", namely, a signal for making a fine adjustment to the valve speed at which the valve body 120 is fully open, has been formed between "h" and "i".

When the valve closing solenoid drive signal s26 is turned OFF at "i", being triggered by a trigger signal (channel 2 signal) at a trailing edge of the signal, a valve opening hold signal "F" composed of a PWM signal is output during a specified period t10. This specified period t10 is determined in the same manner as t5. Thus, the valve body 120 is kept fully open until "j".

As described above, according to the first embodiment, since the width of the valve closing acceleration signal "A" and the seating speed adjusting signal "B" are determined by the position of the valve body 120,

when the travelling speed of the valve body 120 is lowered due to a voltage drop of the battery or an increase of resistance of electromagnetic coils caused by temperature rise for example, the elongated applying time of the drive signal compensates for the travelling speed of the valve body 120.

Especially, when the valve is seated, the elongated applying time of the drive signal compensates the seating speed of the valve body 120, thereby inadequate seatings or void seatings can be prevented.

Further, since the micro-computer 71 has such small functions as supplying when needed the digital data to the DA conversion circuit 212 and the valve hold time data to the timer circuit 213, respectively and since the valve drive control is relied upon the actuator control apparatus 210 but not upon the micro-computer 71, it is possible to lessen a burden on the micro-computer 71 substantially.

Next, a second embodiment of the present invention will be described. The feature of the second embodiment is to determine a timing for turning the valve seating velocity adjusting signal "B" off based on an elapsed time since the valve seating velocity adjusting signal "B" is turned ON, but not on a position of the valve body 120 and an object of the second embodiment is to reduce the seating speed of the valve body 120.

In case of determining the OFF timing of the valve seating velocity adjusting signal "B" by the lift value, if the duration of the valve seating velocity adjusting signal "B" is elongated due to an insufficient acceleration of the armature 150 by the valve opening acceleration signal "A", it is likely that the seating speed becomes rather large due to the further acceleration of the valve seating velocity adjusting signal "B". In this case, the valve closing acceleration signal "A" must be adjusted so that the valve body 120 has a travelling speed larger than a given value.

In the second embodiment, the control for reducing the seating speed is performed by the actuator control apparatus 210. The construction and operation will be described with reference to Fig. 8 and Fig. 9.

Fig. 8 is a block diagram of the system according to the second embodiment and Fig. 9 is a timing chart showing the ON-OFF operation of signals s1 through s24 in the valve control signal output section 214 illustrated in Fig. 8. The components of the second embodiment shown in Fig. 8 which are identical to those of the first embodiment shown in Fig. 5 are denoted by identical reference numerals and are not described in detail.

A signal s14 is a valve closing solenoid drive signal to be output to the valve closing solenoid drive circuit 45a and a signal s24 is a valve opening solenoid drive signal to be output to the valve opening solenoid drive circuit 45b. As shown in Fig. 8, when it is judged that the analogue signal "v" exceeds a reference analogue signal v3, a trigger signal (channel 3) is output to the timer circuit 213.

Then, the timer circuit 213 outputs a signal s9 for

specified period t4. Therefore, the valve seating velocity adjusting signal "B" is turned ON at "c" and, after a specified period t4 elapses, it turned OFF. Similarly, the valve opening velocity adjusting signal "E" is turned ON at "h" and turned OFF after a specified period t9 elapses. These specified periods t4 and t9 are determined in the micro-computer 71 based on the engine operating conditions.

Accordingly, in this embodiment, the valve seating velocity adjusting signal "B" is turned OFF after a specified period t4 elapses since "c" in contrast to the first embodiment where the valve seating velocity adjusting signal "B" is turned OFF at "d" and at the same time the valve closing hold signal "C" is turned ON and only valve closing hold signal "C" is turned ON at "d". Further, the valve opening velocity adjusting signal "E" is turned OFF after a specified period t9 elapses since "h" and only valve opening hold signal "F" is turned ON at "i".

Thus, a period during which the valve seating velocity adjusting signal "B" is turned ON can be shortened and the seating speed of the valve body 120 can be substantially reduced. Further, the valve opening speed also can be reduced largely.

Immediately before the seating velocity adjusting signal "B" is turned OFF, the rate of change of the analogue signal "v" of the lift sensor 170 is small, because the timing when the valve seating velocity adjusting signal "B" is turned OFF is located at an area just before the valve body 120 is seated. Therefore, in case where the noise level of the analogue signal "v" is relatively large, the pulse width tends to vary or the chattering phenomenon is caused easily. However, according to this second embodiment, since the OFF timing of the valve seating velocity adjusting signal "B" is controlled by time, such defects can be eliminated.

Next, describing a third embodiment of the present invention, the feature of the third embodiment is to determine the ON timing of the valve closing acceleration signal "A" by an elapsed time since the OFF timing of the valve opening hold signal "F" and its object is to stabilize the ON timing of the valve closing acceleration signal "A" and also that of the valve opening acceleration signal "D".

Generally, since the electromagnetic generating means 130 comprises a magnetic solenoid including a magnetic core, even if the magnetic solenoid is deenergized, the electromagnetic force does not disappear instantly due to the hysteresis characteristic of the magnetic core.

That is to say, when the valve closing hold signal "C" is turned OFF and then the valve opening acceleration signal "D" is turned ON, the velocity of the valve body 120 is reduced due to the residual attraction force of the valve closing coil 131. Similarly, the velocity of the valve body 120 is reduced due to the residual attraction force of the valve opening solenoid 132. Hence, the gradient of the analogue signal "v" becomes small as much

at "a" and "f".

Because of this, in case where the noise level of the analogue signal "v" is relatively large, the ON timing of the valve closing acceleration signal "A" shows variations or chatterings are caused.

Fig. 10 is a block diagram of the third embodiment and Fig. 11 is a timing chart of signals s1 through s26 in the valve control signal output section 214 shown in Fig. 10. In Fig. 11, the signal s14 is a valve closing solenoid drive signal to be output to the valve closing solenoid drive circuit 45a and the signal 26 is a valve opening solenoid drive signal to be output to the valve opening solenoid drive circuit 45b. The components of the third embodiment shown in Fig. 10 which are identical to those of the first embodiment shown in Fig. 5 are denoted by identical reference numerals and are not described in detail.

In Fig. 10, when it is judged in the comparison circuit 212 that the analogue signal "v" of the lift sensor 170 becomes larger than the reference analogue signal v4, ch1 and ch3 trigger signals are input to the timer circuit 213, respectively.

Then, as indicated in Fig. 11, the timer circuit 213 outputs a ch1 output signal s11 for a specified period t5 and at the same time outputs an inverted ch3 output s15 for a specified period t5 + t6.

Therefore, the valve opening acceleration signal "D" is turned ON (time "f") after a specified period t6 has elapsed since the valve closing hold signal "C", is turned OFF (time "e").

Similarly, the valve closing acceleration signal "A" is turned ON (time "a") after a specified period t11 has elapsed since the valve opening hold signal "F" is turned OFF (time "j"). These specified periods of time t6 and t11 are determined in the micro-computer 71 according to the engine operating conditions.

Accordingly, the ON timing of the valve closing acceleration signal "A" can be determined based on the elapsed time since the valve opening hold signal "F" is turned OFF. Similarly, the ON timing of the valve opening acceleration signal "D" can be determined according to the elapsed time since the valve closing hold signal "C" is turned OFF. Thus, the ON timing of the valve closing acceleration signal "A" and the ON timing of the valve opening acceleration signal "D" can be stabilized and this results in preventing variations of the ON timing of the valve closing acceleration signal "A" and the valve opening acceleration signal "D" or eliminating chatterings of the valve body 120.

Next, describing a fourth embodiment of the present invention, the fourth embodiment is characterized in that the OFF timing of the valve closing acceleration signal "A" and that of the valve opening acceleration signal "D" are determined by an elapsed time since the valve closing acceleration signal "A" and the valve opening acceleration signal "D" are turned ON, but not by the position of the valve body 120 and its object is to prevent the electromagnetic solenoid from

burning due to inadequate seatings.

In case of determining the OFF timing of the valve closing acceleration signal "A" or the valve opening acceleration signal "D" based on the position of the valve body 120, there is a possibility that the period during which the valve closing acceleration signal "A" or the valve opening acceleration signal "D" is turned ON is elongated, when the valve body 120 is seated or open insufficiently.

It is an object of this embodiment to prevent the electromagnetic solenoid from burning at the event of insufficient seating of the valve body by providing a threshold value in the 'ON' period.

Fig. 12 is a block diagram of the valve control system according to the fourth embodiment and Fig. 13 is a timing chart of signals s1 through s24 in the valve control signal output section 214 shown in Fig. 12. The signal s13 in Fig. 13 is a valve closing solenoid drive signal to be output to the valve closing solenoid drive circuit 45a and the signal s24 is a valve opening solenoid drive signal to be output to the valve opening solenoid drive circuit 45b. The components of the fourth embodiment shown in Fig. 12 which are identical to those of the first embodiment shown in Fig. 5 are denoted by identical reference numerals and are not described in detail.

Referring to Fig. 12, when it is judged in the comparison circuit 212 that the analogue signal "v" of the lift sensor 170 becomes larger than the reference analogue signal "v", a ch3 trigger signal is input to the timer circuit 213 and then, as indicated in Fig. 13, the timer circuit 213 outputs a ch3 output signal s2 for a specified period t2.

Accordingly, the valve closing acceleration signal "A" is turned OFF after a specified period t2 has elapsed since it is turned ON (time "a"). Similarly, the valve opening acceleration signal "D" is turned OFF after a specified period t7 has elapsed since it is turned ON (time "f"). These periods of time t2 and t7 are determined in the micro-computer 71 according to the engine operating conditions. Namely, the OFF timing of the valve closing acceleration signal "A" can be determined by an elapsed time since the valve closing acceleration signal "A" is turned ON and also the OFF timing of the valve opening acceleration signal "D" can be determined by an elapsed time since the valve opening acceleration signal "D" is turned ON. Thus, it is possible to prevent the electromagnetic solenoid from burning by restricting current passing through the valve closing solenoid 131 or the valve opening solenoid 132 in the event of inadequate seating of the valve body.

In summary, the electromagnetically operated valve control system according to the present invention can alleviate a burden on the micro-computer (central computing and processing means) and perform a more sophisticated control to numerous electromagnetic valves. Therefore, it is possible to reduce the size of the micro-computer and also to lower the cost thereof. Further, the seating control of the valve body which is one

of the features of this valve control system can improve durability and quietness of the system.

While the presently preferred embodiments of the present invention have been shown and described, it is to be understood that these disclosures are for the purpose of illustration and that various changes and modifications may be made without departing from the scope of the invention as set forth in the appended claims.

Claims

1. An electromagnetically operated valve control system for an engine (10) having a combustion chamber (31), a valve body (120) reciprocating between a fully closed position and a fully open position so as to open and close the combustion chamber (31), an actuator (44) connected with the valve body (120) for driving the valve body by energizing and deenergizing a valve closing solenoid (131) and a valve opening solenoid (132), and an actuator drive circuit (45) for energizing and deenergizing the valve closing solenoid (131) and the valve opening solenoid (132) of the actuator (44), comprising:

control data generating means (70) for generating control data based on operating conditions of the engine (10);

valve position detecting means (170) for detecting reference positions of the valve body (120);

valve closing acceleration means (210) for energizing the valve closing solenoid (131) when the valve body (120) passes a first reference position established apart from the fully open position and for deenergizing the valve closing solenoid (131) when the valve body (120) passes a second reference position closer to the fully closed position than the first reference position;

valve seating velocity adjusting means (210) for energizing the valve closing solenoid (131) when the valve body (120) passes a third reference position closer to the fully closed position than the second reference position and for deenergizing the valve closing solenoid (131) when the valve body (120) passes a fourth reference position closer to the fully closed position than the third reference position so as to adjust a seating velocity of the valve body (120); and

valve closing hold means for repeatedly energizing and deenergizing the valve closing solenoid (131) when the valve body (120) passes the fourth reference position and for deenergizing the valve closing solenoid (131) when a first specified period has elapsed since the valve body (120) passes the fourth reference position.

2. The system according to claim 1, further comprising:

valve opening acceleration means (210) for energizing the valve opening solenoid (132) when the valve body (120) passes a fifth reference position apart from the fully closed position and for deenergizing the valve opening solenoid (132) when the valve body (120) passes a sixth reference position closer to the fully open position than the fifth reference position;

valve opening velocity adjusting means (210) for energizing the valve opening solenoid (132) when the valve body (120) passes a seventh reference position closer to the fully open position than the sixth reference position and for deenergizing the valve opening solenoid (132) when the valve body (120) passes an eighth reference position closer to the fully open position than the seventh reference position so as to adjust an opening velocity of the valve body; and

valve opening hold means for repeatedly energizing and deenergizing the valve opening solenoid (132) when the valve body (120) passes the eighth reference position and for deenergizing the valve closing solenoid (131) when a second specified period has elapsed since the valve body (120) passes the eighth reference position so as to hold the valve body (120) at the fully open position.

3. The system according to claim 1 or 2, wherein the control data include data of the first specified period and the reference positions comprise the first reference position, the second reference position, the third reference position and the fourth reference position.
4. The system according to claim 2 or 3, wherein the control data include data of the second specified period and the reference positions comprise the eighth reference position, the sixth reference position, the seventh reference position and the eighth reference position.
5. The system according to any of claims 1 to 4, wherein the valve seating velocity adjusting means energize the valve closing solenoid (131) when the valve body (120) passes the third reference position and deenergize the valve closing solenoid (131) when a third specified period has elapsed since the valve body (120) passes the third reference position so as to adjust a seating velocity of the valve body (120).
6. The system according to any of claims 2 to 5,

wherein the valve opening velocity adjusting means energize the valve opening solenoid (132) when the valve (120) passes the seventh reference position and deenergize the valve opening solenoid (132) when a fourth specified period has elapsed since the valve body (120) passes the seventh reference position so as to adjust an opening velocity of the valve body.

and deenergizing a valve closing solenoid (131) and a valve opening solenoid (132), and an actuator drive circuit (45) for energizing and deenergizing the valve closing solenoid (131) and the valve opening solenoid (132) of the actuator (44), comprising:

7. The system according to any of claims 1 to 6, wherein the valve closing acceleration means (210) energize the valve closing solenoid (131) when a fifth specified period has elapsed since the valve opening solenoid (132) is deenergized and deenergize the valve closing solenoid (131) when the valve body (120) passes the second reference position.
8. The system according to any of claims 1 to 7, wherein the valve opening acceleration means (210) energize the valve opening solenoid (132) when a sixth specified period has elapsed since the valve closing solenoid (131) is deenergized and deenergize the valve opening solenoid (132) when the valve body (120) passes the sixth reference position.
9. The system according to any of claims 1 to 8, wherein valve closing acceleration means (210) energize the valve closing solenoid (131) when the valve body (120) passes the first reference position and deenergize the valve closing solenoid (131) when a seventh specified period has elapsed since the valve body (120) passes the first reference position.
10. The system according to any of claims 1 to 9, wherein valve opening acceleration means (210) energize the valve opening solenoid (132) when the valve body (120) passes the fifth reference position and deenergize the valve opening solenoid (132) when an eighth specified period has elapsed since the valve body (120) passes the fifth reference position.
11. The system according to any of claims 5 to 10, wherein the third specified period, the fourth specified period, the fifth specified period, the sixth specified period, the seventh specified period, and the eighth specified period are included in the control data.
12. An electromagnetically operated valve control system for an engine (10) having a combustion chamber (31), a valve body (120) reciprocating between a fully closed position and a fully open position so as to open and close the combustion chamber (31), an actuator (44) connected with the valve body (120) for driving the valve body (120) by energizing

a computer (71) for generating control data based on operating conditions of the engine (10); and

an actuator control apparatus (210) separately provided from the computer (71) for controlling the actuator drive circuit (45).

13. The system according to claim 12, wherein the actuator control apparatus (210) includes a position detecting section (170) for detecting a position of the valve body (120), a valve control signal output section (214) for outputting a control signal to operate the actuator drive circuit (45) and a timer circuit (213) for determining an output timing of the control signal based on the position of the valve body (120).

14. The system according to claim 13, wherein the position detecting section includes a lift sensor (170) for outputting the position of the valve body (120) as an analogue signal, a digital-to-analogue conversion circuit (211) for converting a digital signal from the computer (70) into a reference analogue signal corresponding to the position of the valve body (120), and a comparison circuit (212) for comparing the reference analogue signal with the analogue signal output from the lift sensor.

15. An electromagnetically operated valve control method for an engine (10) having a combustion chamber (31), a valve body (120) reciprocating between a fully closed position and a fully open position so as to open and close the combustion chamber (31), an actuator (44) connected with the valve body (120) for driving the valve body (120) by energizing and deenergizing a valve closing solenoid (131) and a valve opening solenoid (132), and an actuator drive circuit (45) for energizing and deenergizing the valve closing solenoid (131) and the valve opening solenoid (132) of the actuator (44), comprising the following steps:

generating control data based on operating conditions of the engine (10);

detecting reference positions of the valve body (120);

energizing the valve closing solenoid (131) when the valve body (120) passes a first reference position apart from the fully open position and deenergizing the valve closing solenoid (131) when the valve body (120) passes a sec-

ond reference position closer to the fully closed position than the first reference position; energizing the valve closing solenoid (131) when the valve body (120) passes a third reference position closer to the fully closed position 5 than the second reference position and deenergizing the valve closing solenoid (131) when the valve body (120) passes a fourth reference position closer to the fully closed position than the third reference position so as to adjust a 10 seating velocity of the valve body (120); and repeatedly energizing and deenergizing the valve closing solenoid (131) when the valve body (120) passes the fourth reference position and deenergizing the valve closing solenoid 15 (131) when a first specified period has elapsed since the valve body (120) passes the fourth reference position.

16. The method according to claim 15, 20 further comprising the following steps:

energizing the valve opening solenoid (132) when the valve body (120) passes a fifth reference position apart from the fully closed position 25 and deenergizing the valve opening solenoid (132) when the valve body (120) passes a sixth reference position closer to the fully open position than the fifth reference position; 30 energizing the valve opening solenoid (132) when the valve body (120) passes a seventh reference position closer to the fully open position than the sixth reference position and deenergizing the valve opening solenoid (132) when 35 the valve body (120) passes an eighth reference position closer to the fully open position than the seventh reference position so as to adjust an opening velocity of the valve body (120); and 40 repeatedly energizing and deenergizing the valve opening solenoid (132) when the valve body (120) passes the eighth reference position and deenergizing the valve closing solenoid (131) when a second specified period has 45 elapsed since the valve body (120) passes the eighth reference position so as to hold the valve body (120) at the fully open position.

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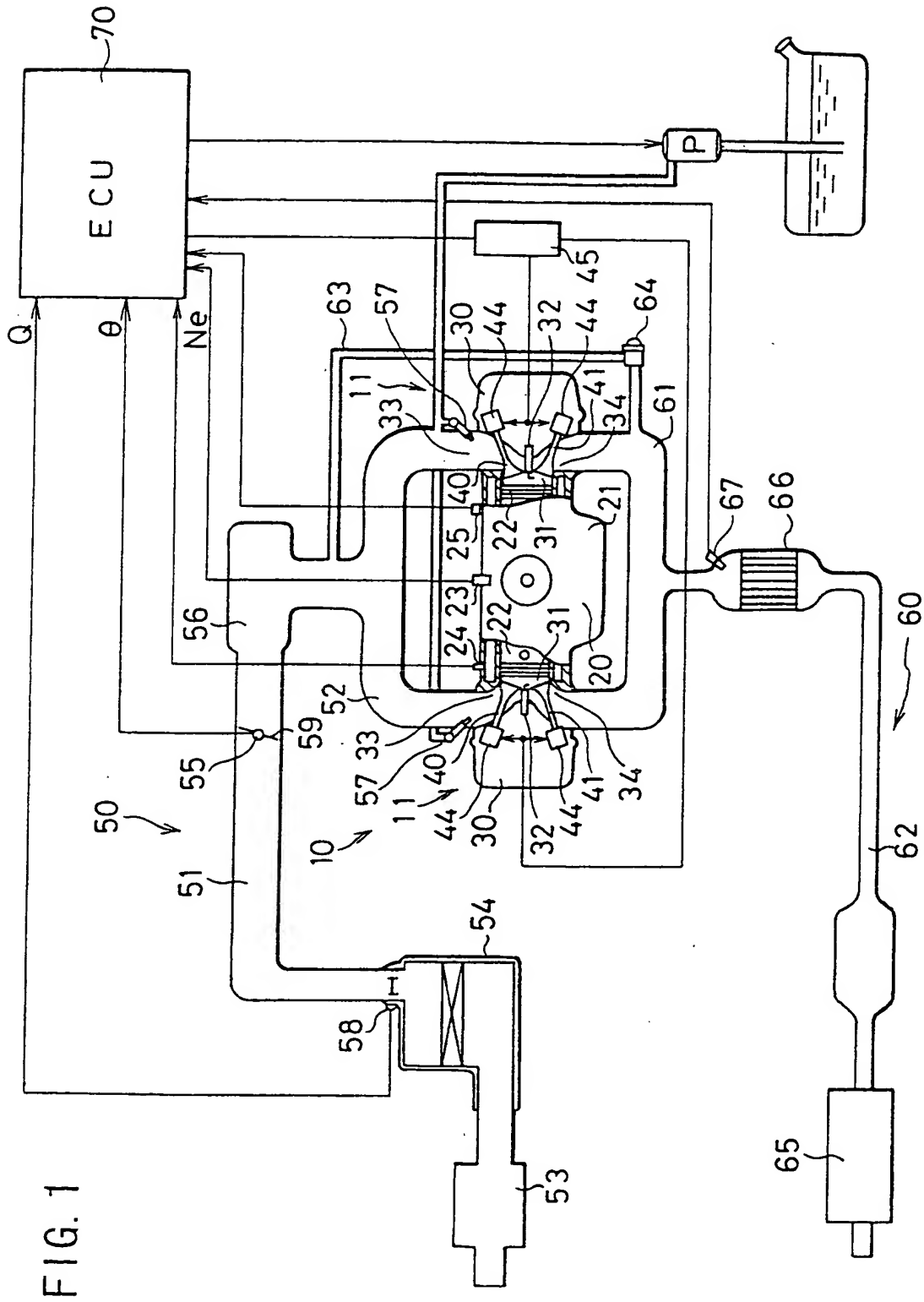


FIG. 2

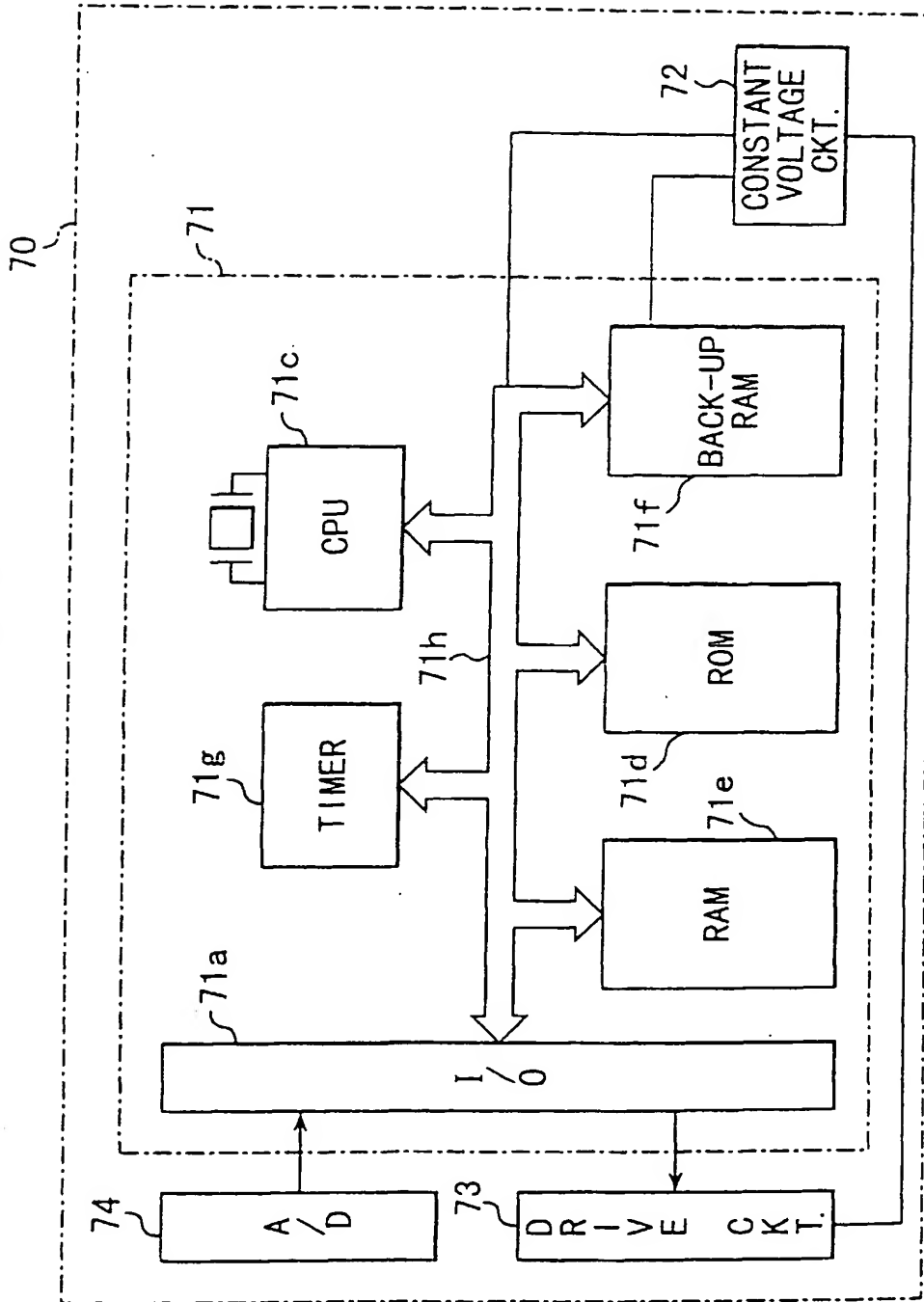


FIG. 3

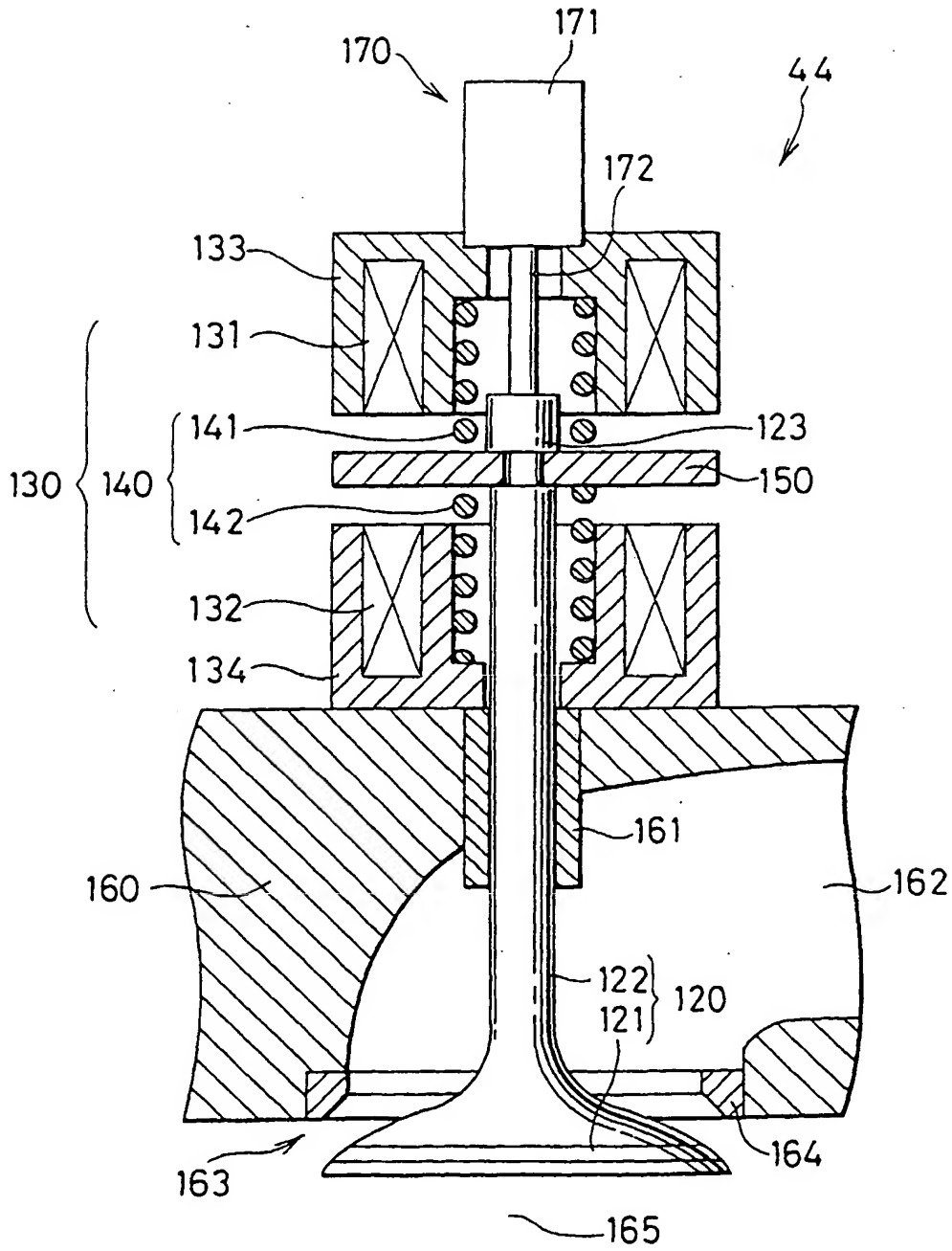


FIG. 4

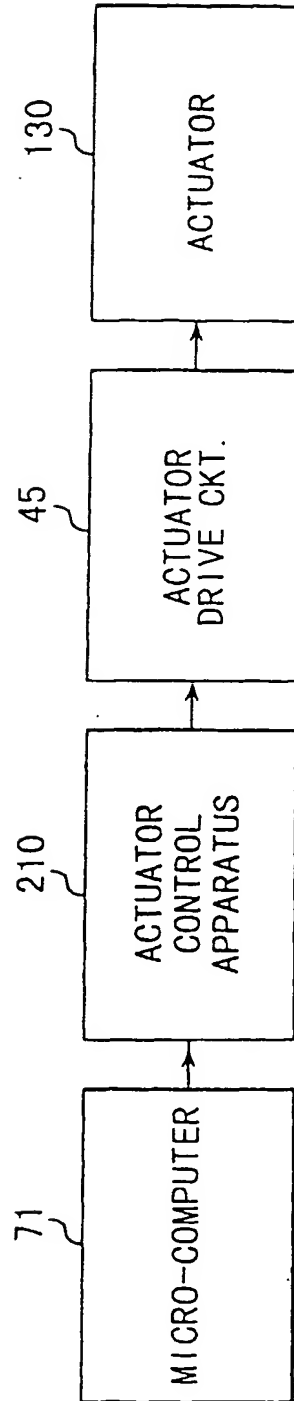


FIG. 5

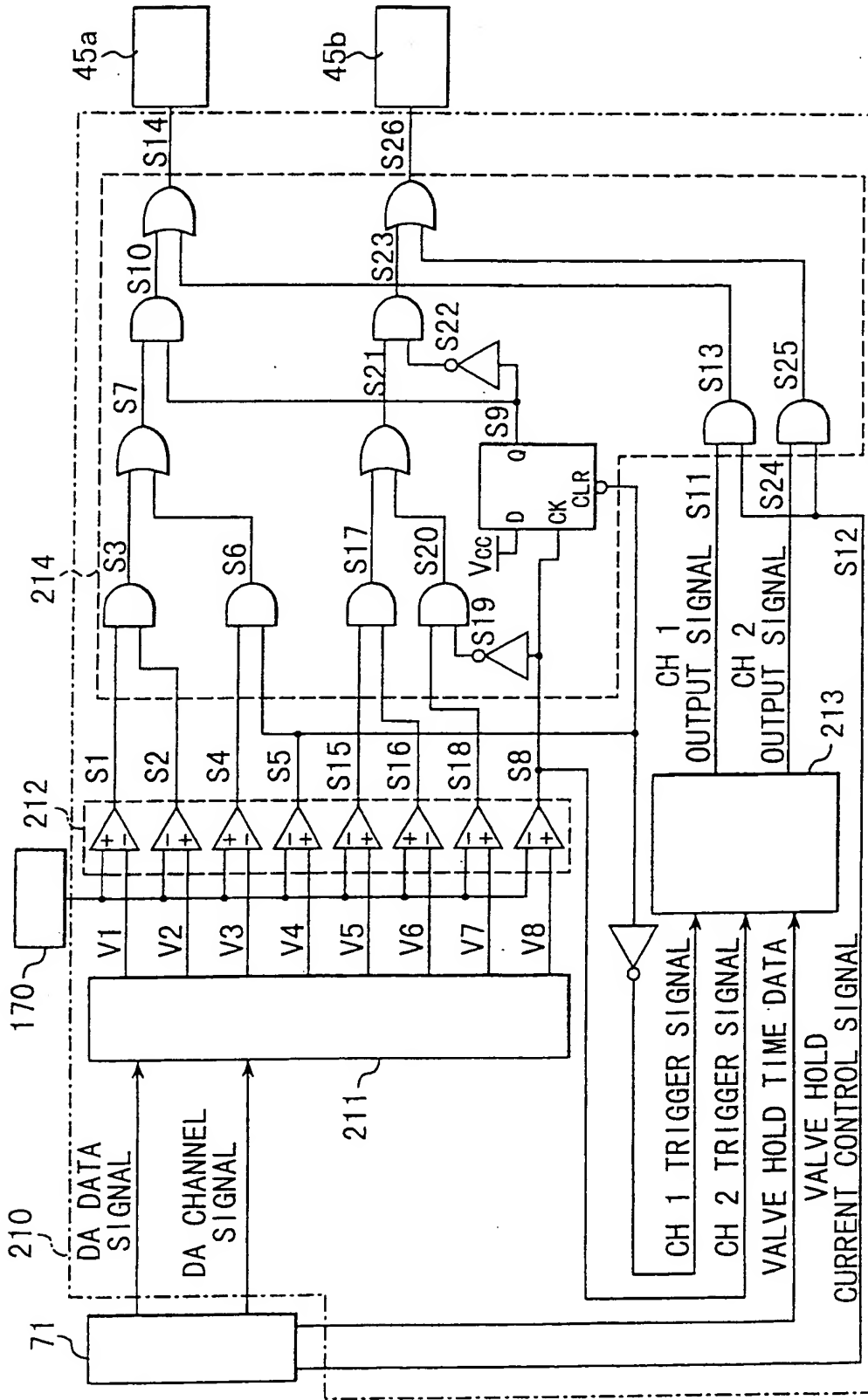


FIG. 6

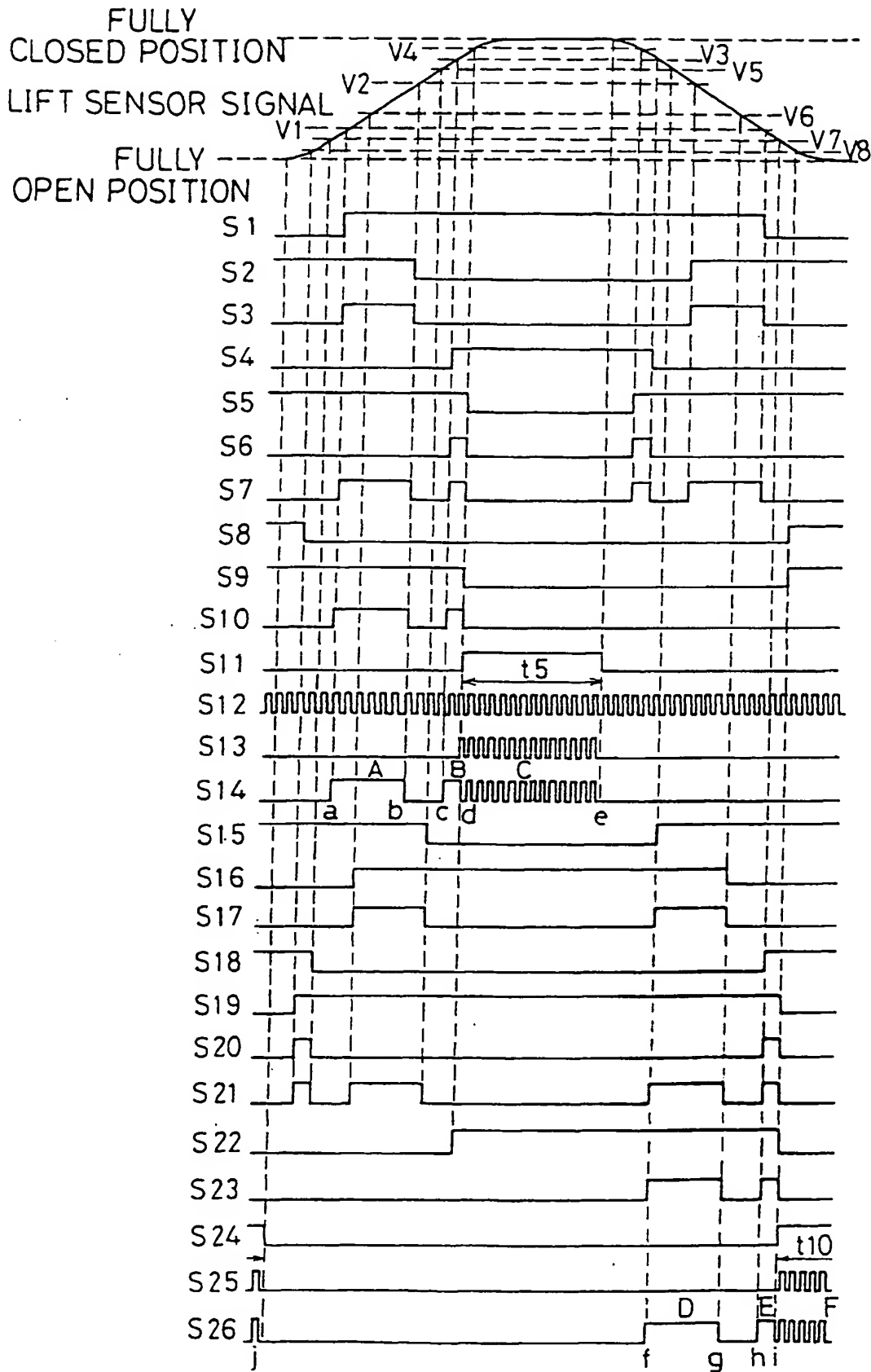


FIG. 7

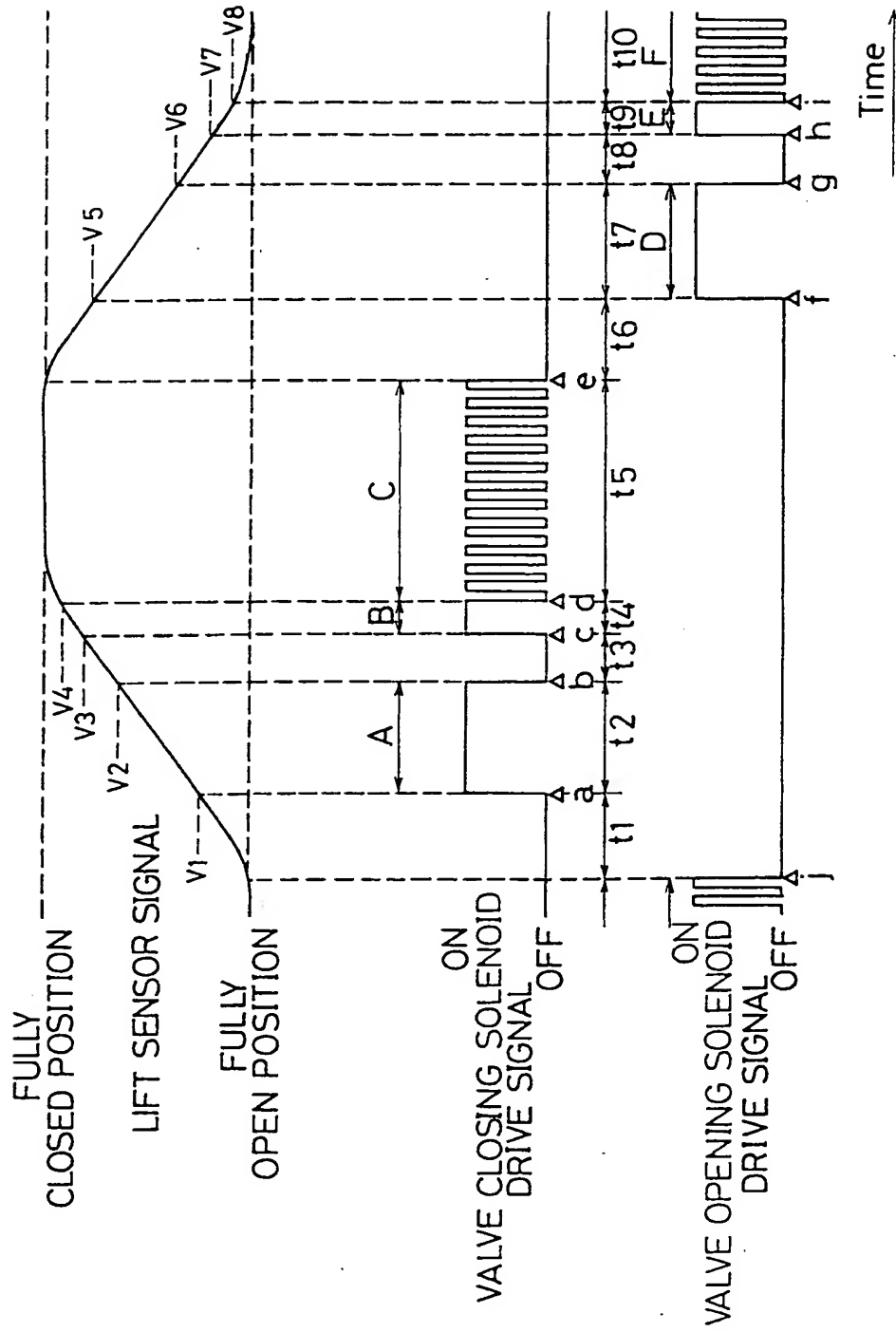


FIG. 8

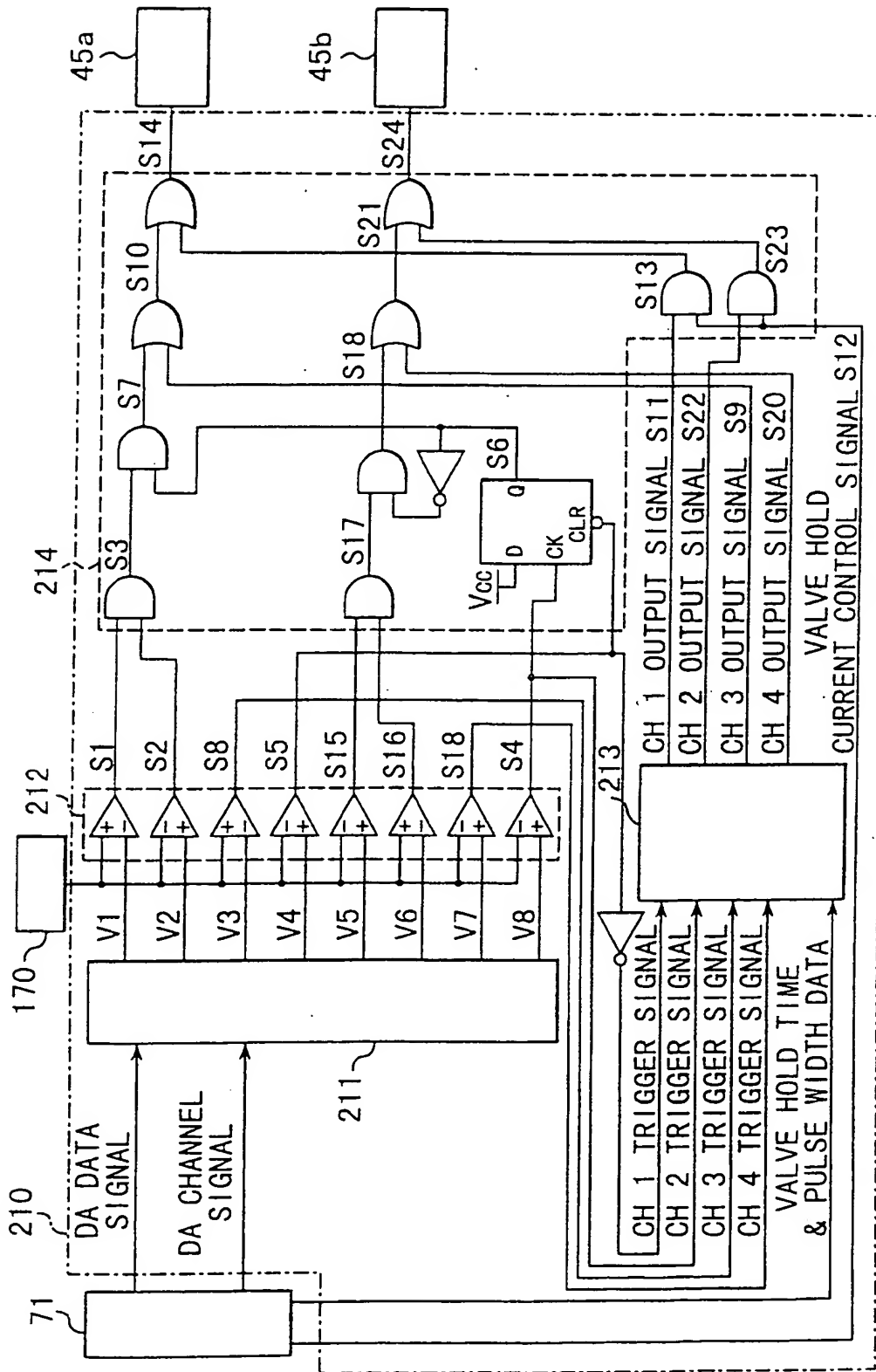


FIG. 9

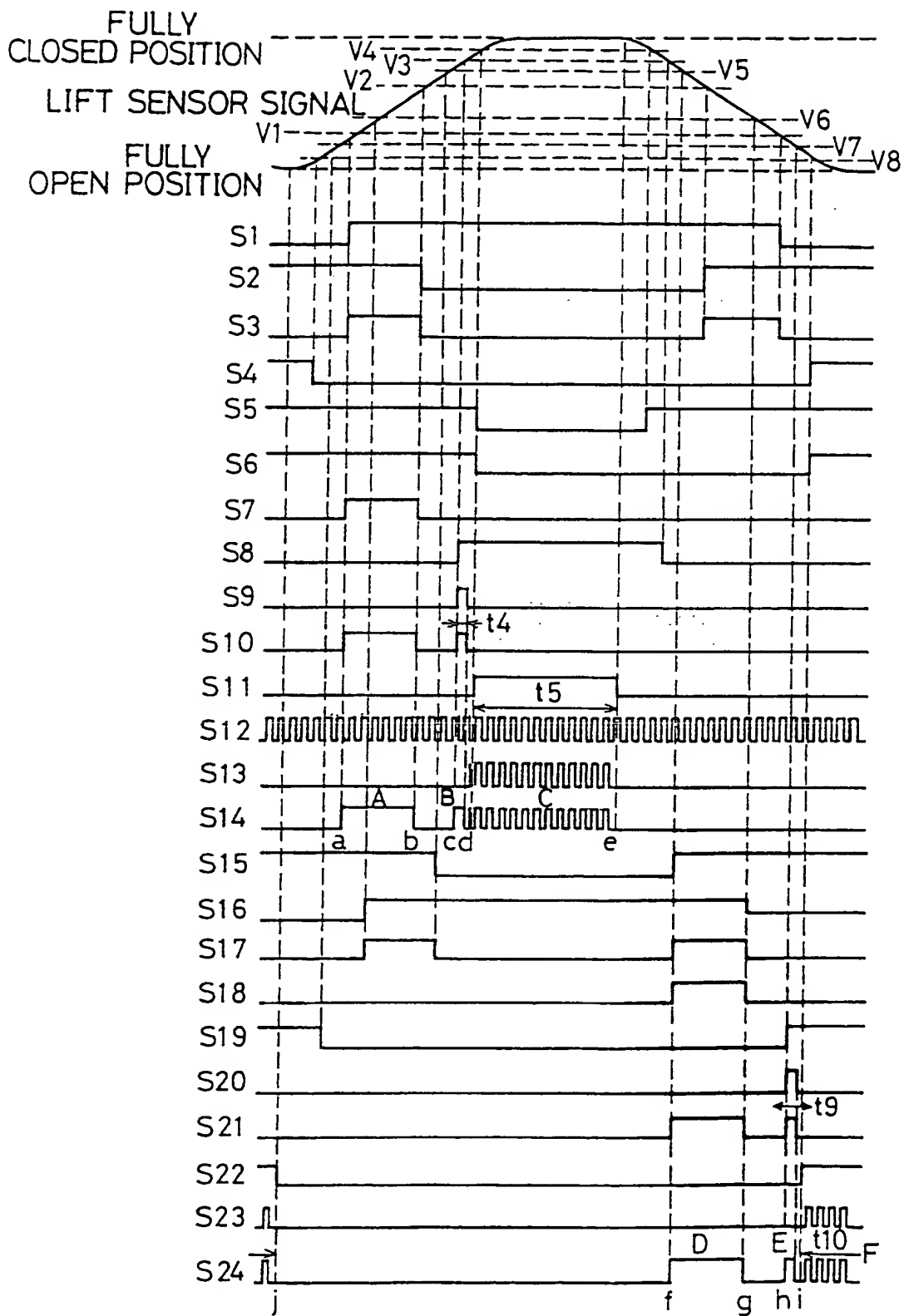


FIG. 10

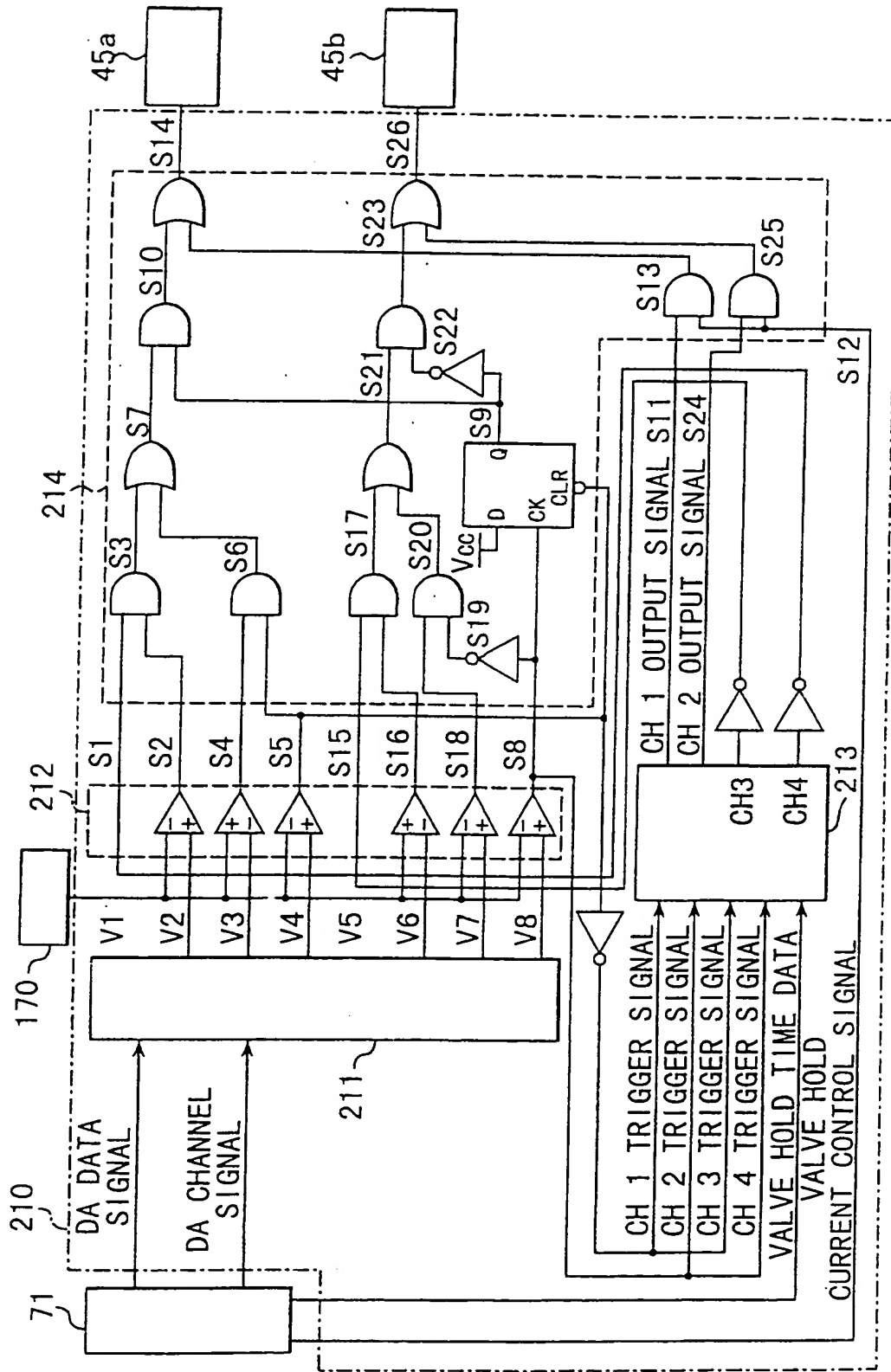


FIG. 11

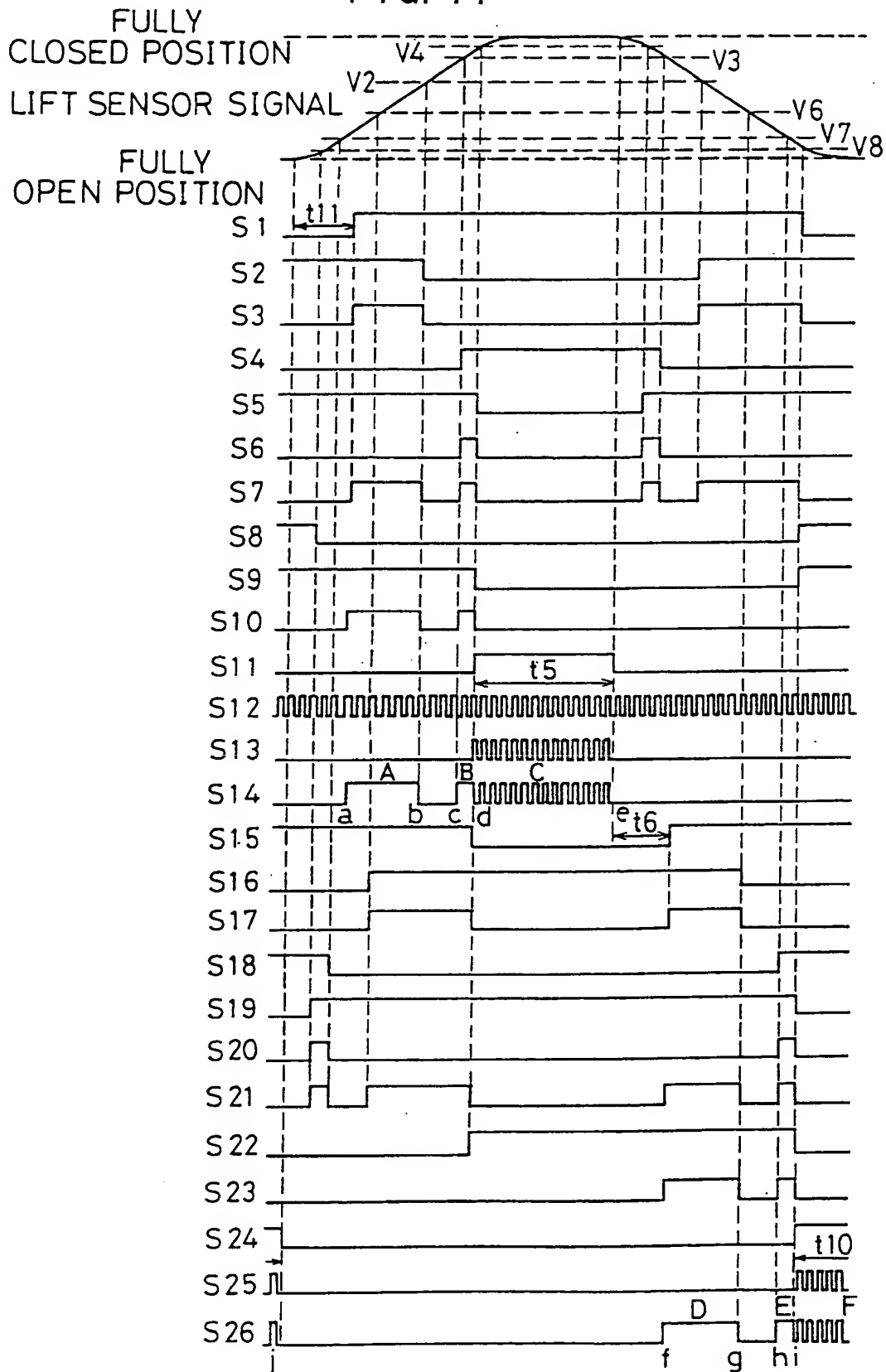


FIG. 12

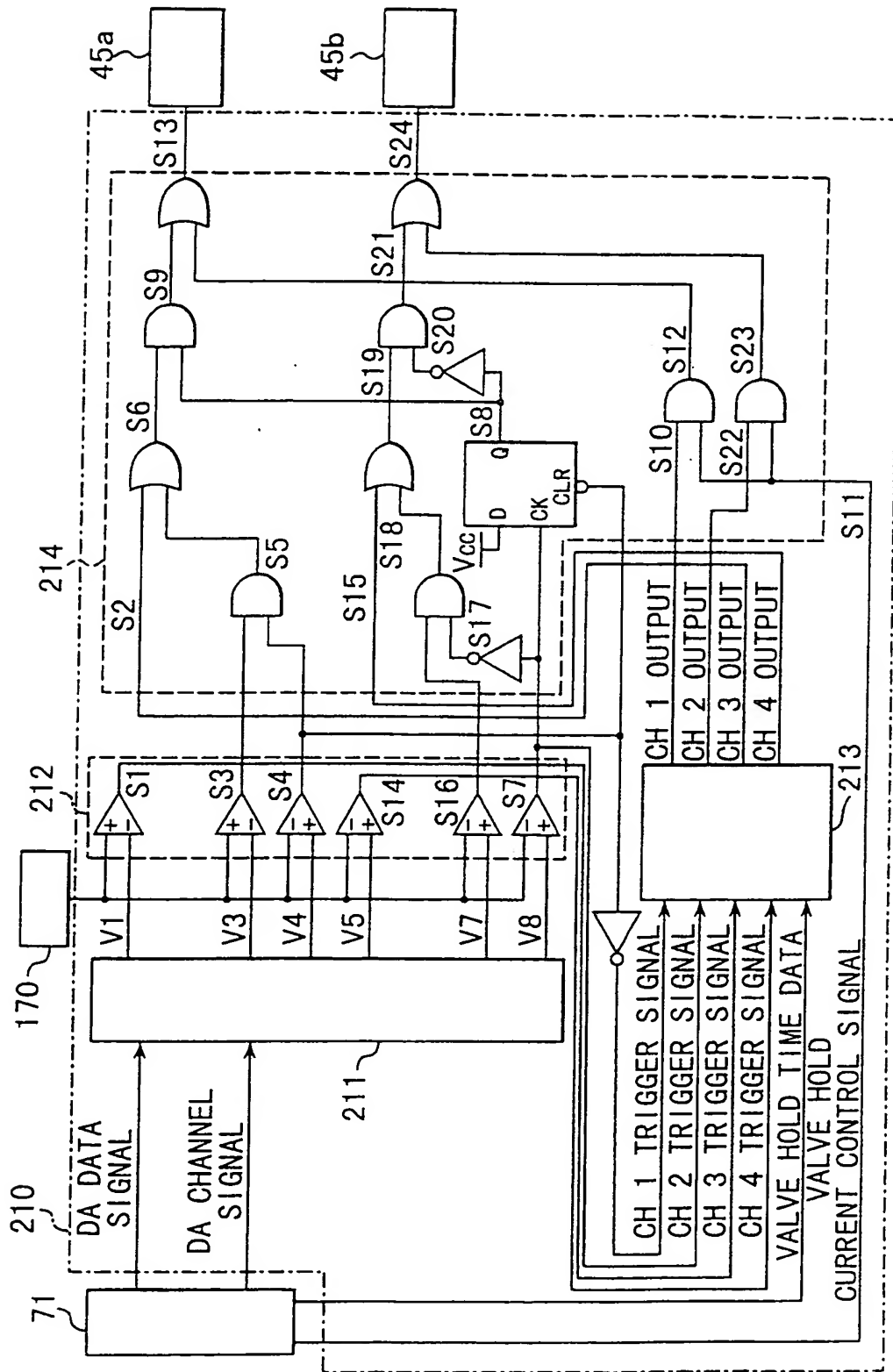


FIG. 13

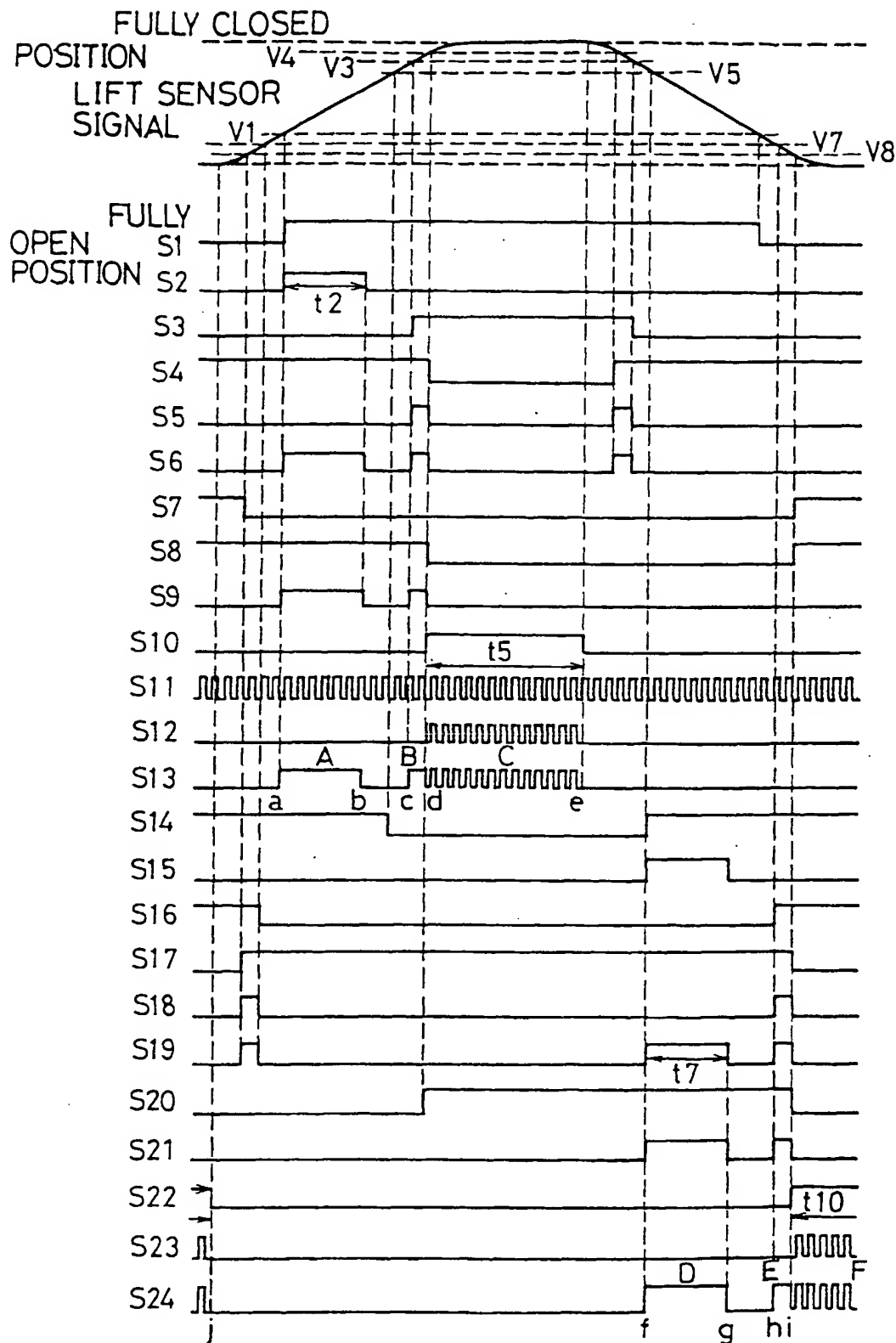
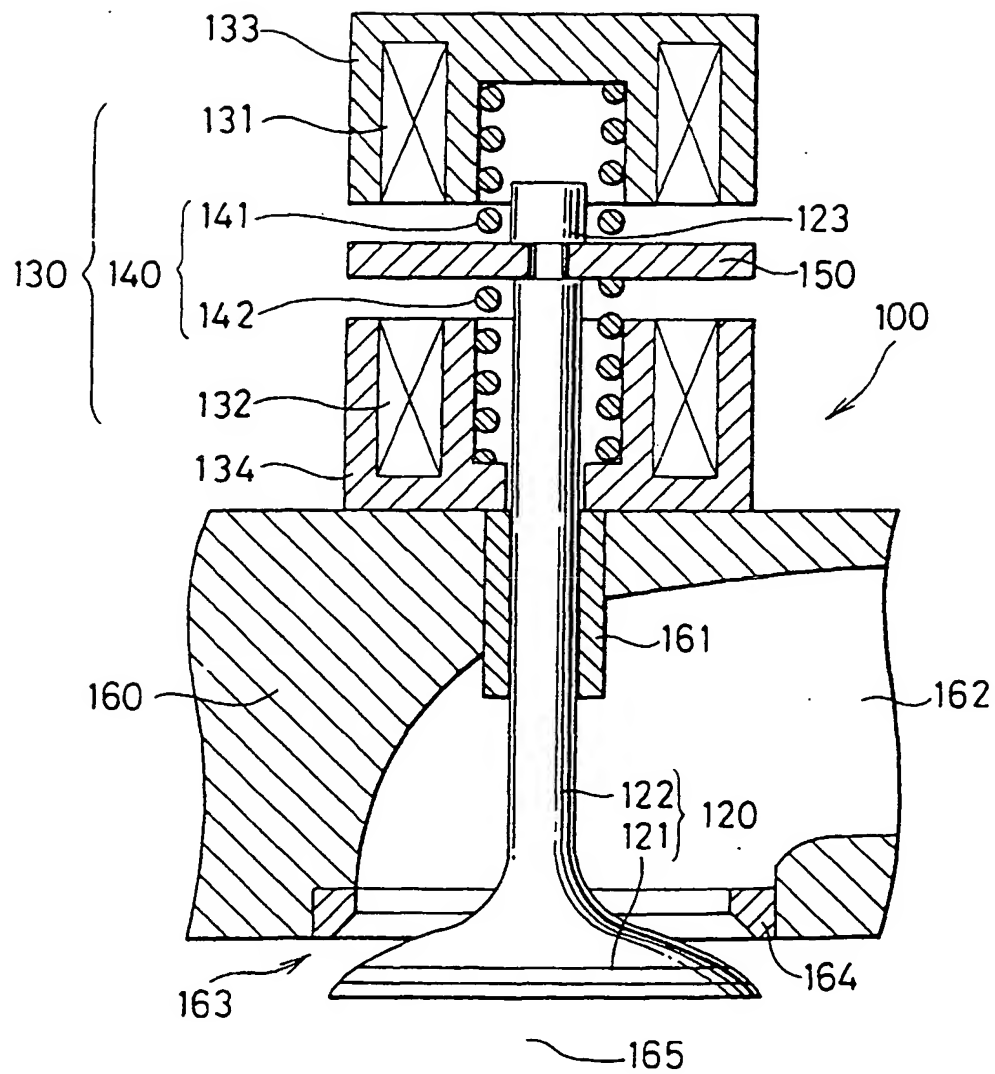


FIG. 14





European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 98 10 5675

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	EP 0 724 067 A (HONDA MOTOR CO LTD) 31 July 1996 * column 7, line 1 - line 55; figure 2 *	12-14	F01L9/04
A	---	1,15	
X	US 5 201 296 A (WUNNING JOHN J ET AL) 13 April 1993 * column 2, line 64 - column 3, line 7 * * column 3, line 44 - line 49 * * column 3, line 63 - column 4, line 8 * * figures 1,2 *	12-14	
A	---	1,15	
X	WO 92 02712 A (RICHARDS KEITH LESLIE ;ASHEN RICHARD ANTHONY (GB)) 20 February 1992 * page 8, line 15 - page 11, line 2; figures 1-3 *	12-14	
A	---	1,15	
A	US 5 072 700 A (KAWAMURA HIDEO) 17 December 1991 * column 3, line 43 - line 56 * * column 4, line 25 - column 5, line 39 * * figures 1-3 *	1,12,15	TECHNICAL FIELDS SEARCHED (Int.Cl.6) F01L
A	--- "ELECTROMAGNETIC ENGINE VALVE ACTUATOR WITH LOW SEATING VELOCITY" RESEARCH DISCLOSURE, no. 352, 1 August 1993, page 518 XP000395246 -----	1,12,15	
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 26 May 1998	Examiner Lefebvre, L
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

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